

ELEC0047 - Power system dynamics, control and stability

Dynamic simulation of a five-bus system

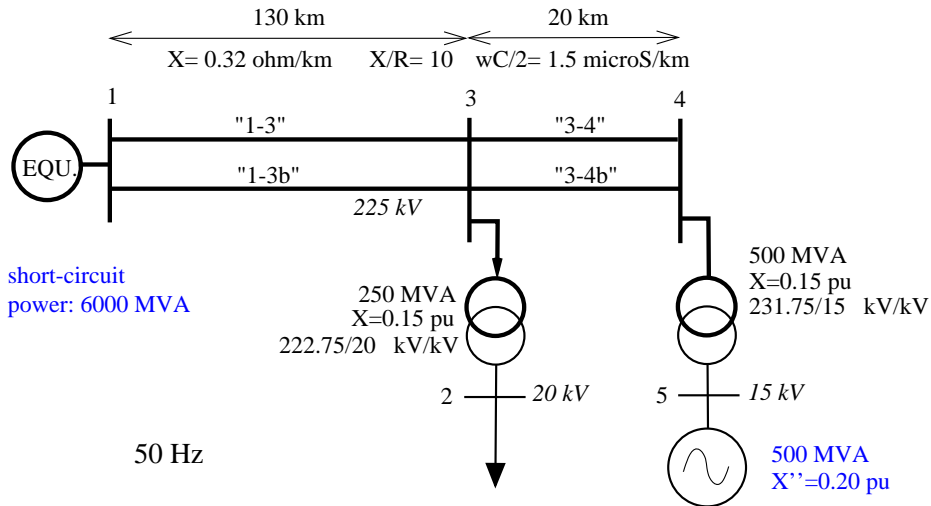
Thierry Van Cutsem

`t.vancutsem@ulg.ac.be`

`www.montefiore.ulg.ac.be/~vct`

November 2017

System modelling and operating points



Load tap changer controlling voltage at bus 2

transformer ratio : minimum : 0.88

maximum : 1.20

number of tap positions : 33

voltage dead-band : $[V^o - 0.01 \quad V^o + 0.01] \text{ pu}$

delay before first tap change : 25 s

between subsequent tap changes : 10 s

Generator G5: synchronous machine data

$$R_a = 0. \quad X_\ell = 0.15 \text{ pu} \quad m = 0.10 \quad n = 6.0257$$

$$X_d = 2.20 \quad X'_d = 0.30 \quad X''_d = 0.20 \text{ pu}$$

$$X_q = 2.00 \quad X'_q = 0.40 \quad X''_q = 0.20 \text{ pu}$$

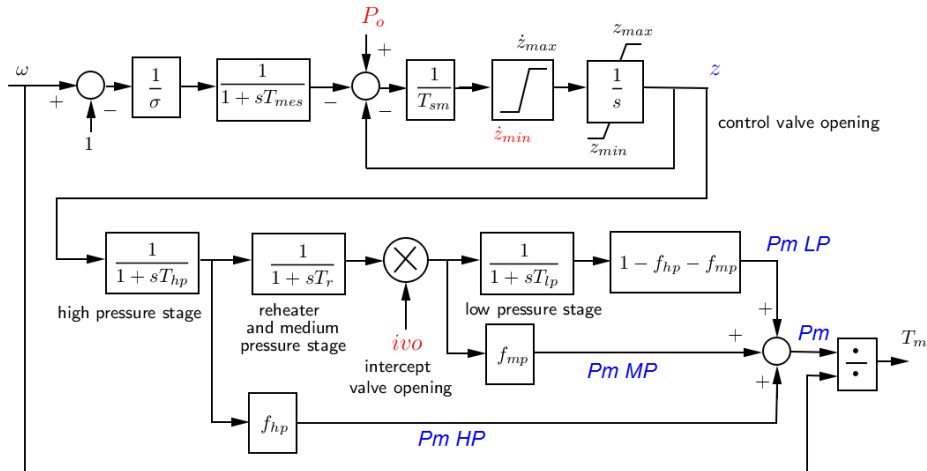
$$T'_{do} = 7.00 \quad T''_{do} = 0.05 \quad T'_{qo} = 1.50 \quad T''_{qo} = 0.05 \text{ s}$$

$$H = 4 \text{ s}$$

(values in pu on the generator 500 MVA base)

Generator G5: speed governor and steam turbine

$$P_{nom} = 460 \text{ MW}$$



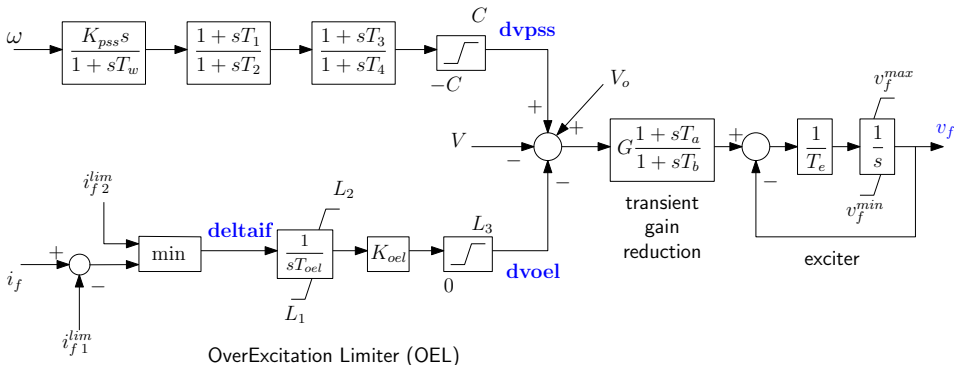
$$\sigma = 0.04 \quad T_{mes} = 0.1 \text{ s} \quad T_{sm} = 0.4 \text{ s}$$

$$\dot{z}_{min} = -0.05 \text{ pu/s} \quad \dot{z}_{max} = 0.05 \text{ pu/s} \quad z_{min} = 0. \quad z_{max} = 1. \text{ pu}$$

$$T_{hp} = 0.3 \text{ s} \quad f_{hp} = 0.4 \quad T_r = 5.0 \text{ s} \quad f_{mp} = 0.3 \quad T_{lp} = 0.3 \text{ s} \quad ivo = 1$$

Generator G5: automatic voltage regulator, excitation system, overexcitation limiter

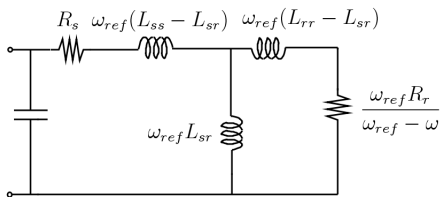
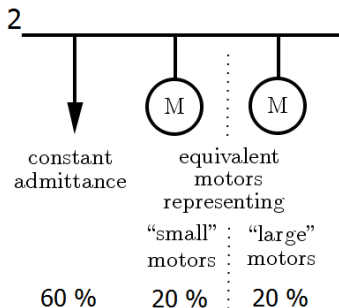
Power System Stabilizer (PSS)



OverExcitation Limiter (OEL)

$$\begin{aligned}
 G &= 70. & T_a &= T_b = 1 \text{ s} & T_e &= 0.4 \text{ s} & v_f^{min} &= 0. & v_f^{max} &= 5 \text{ pu} \\
 K_{pss} &= 50 & T_w &= 5 \text{ s} & T_1 &= T_3 = 0.323 \text{ s} & T_2 &= T_4 = 0.0138 \text{ s} & C &= 0.06 \text{ pu} \\
 i_{f1}^{lim} &= 2.90 \text{ pu} & i_{f2}^{lim} &= 1.00 \text{ pu} & T_{oel} &= 8 \text{ s} & K_{oel} &= 2.0 \\
 L_1 &= -1.1 & L_2 &= 0.1 & L_3 &= 0.2 \text{ pu}
 \end{aligned}$$

Modelling of load at bus 2



Mechanical torque: $T_m = T_{mo}(A\omega^2 + B)$

“small motors”:

$$R_s = 0.031 \quad L_{ss} = 3.30 \quad L_{sr} = 3.20 \quad L_{rr} = 3.38 \quad R_r = 0.018 \text{ pu}$$

$$H = 0.7 \text{ s} \quad A = 0.5 \quad B = 0.5$$

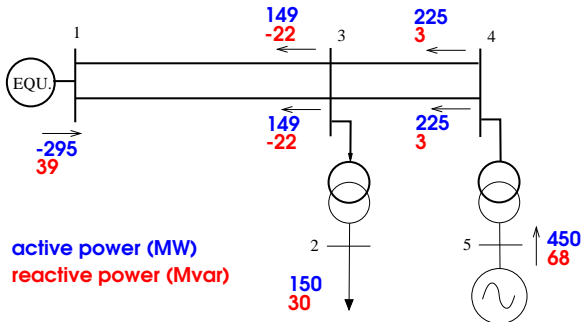
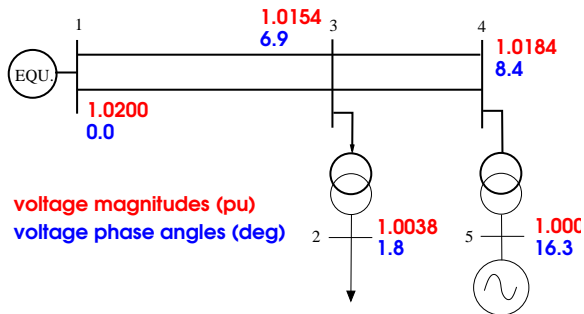
“large motors”:

$$R_s = 0.013 \quad L_{ss} = 3.867 \quad L_{sr} = 3.80 \quad L_{rr} = 3.97 \quad R_r = 0.009 \text{ pu}$$

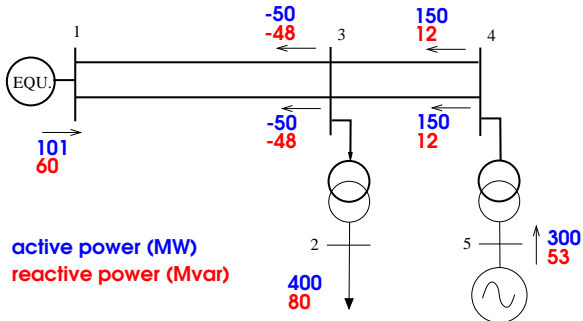
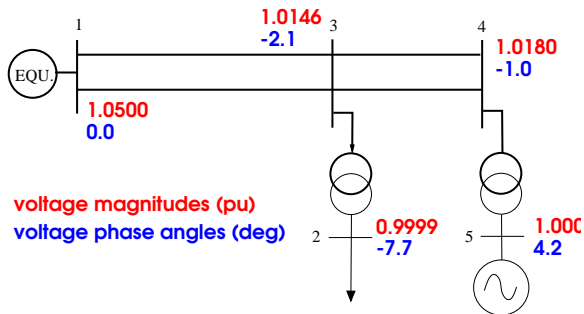
$$H = 1.5 \text{ s} \quad A = 0.5 \quad B = 0.5$$

(values in pu on the motor MVA base)

Operating point # 1



Operating point # 2



Syntax of disturbance file

```
0.000 CONTINUE SOLVER BD 0.010 0.001 0.0 ALL
! add your events here, by increasing order of times.
20.000 STOP
```

To increase the power setpoint of generator G by D pu in T seconds :

```
<time>  CHGPRM  TOR  G  Po  value_of_D  value_of_T
```

To increase the voltage setpoint of generator G by D pu in T seconds :

```
<time>  CHGPRM  EXC  G  Vo  value_of_D  value_of_T
```

To increase the value of the Thévenin voltage by D pu in T seconds :

```
<time>  CHGPRM  INJ  EQUIV1  ETH  value_of_D  value_of_T
```

To apply a fault at bus B with resistance R and reactance X (in Ω , can be zero) :

```
<time>  FAULT  BUS  B  value_of_R  value_of_X
```

To clear a fault at bus B :

```
<time>  CLEAR  BUS  B
```

To trip line XYZ:

```
<time>  BREAKER  BRANCH  XYZ  0  0
```

Case 1

- Operating point : # 2
- disturbance : at $t = 1$ s, increase of power set-point P_o by 115 MW in 10 s^{-1}
- simulated time : 60 s.

Comment as far as possible the evolution of :

- the generator active power
- the generator reactive power
- the generator rotor angle
- the generator field current
- the control valve z of the turbine
- the voltage magnitude at bus 3.

¹power ramping are much slower in real life !

Case 2

- Operating point : # 1
- disturbance : at $t = 1$ s, increase of voltage set-point V_o by 0.05 pu in 2 s
- simulated time : 60 s.

Comment as far as possible the evolution of :

- the voltage magnitude at bus 3. In particular, explain the three “spikes” with the help of the proper curves
- the generator active power
- the generator reactive power
- the generator field current.

Case 3

- Operating point : # 1
 - disturbance : at $t = 1$ s, “voltage dip” in the external system simulated by a decrease of the Thévenin voltage by 0.20 pu during 0.04 s
(*can be seen considered as an impulse response*)
 - simulated time : 20 s.
-
- Observe the evolution of the rotor speed of the generator
 - Observe the evolution of the PSS output
(*select: generator G5 - observable of excitation control - dvpss*)
 - take the Power System Stabilizer (PSS) out of service, simulate the same disturbance and compare the evolution of the rotor speed with the previous one
 - observe the evolution of the voltage magnitude at bus 3 and comment on the similarity
 - what is the period of the dominant oscillation ?

Put the PSS back in service !

Case 4

- Operating point : # 1
- disturbance : at $t = 1$ s, a solid fault on line 1-3, cleared after 4 cycles (0.08 s) by opening the faulted circuit. The fault takes place very near bus 3, so that it can be applied at bus 3
- simulated time : 20 s.

Comment as far as possible the evolution of :

- the terminal voltage of the generator
- the active and reactive powers of the generator
- the rotor speed of the generator
- the field voltage of the generator
(*select: generator G5 - observable of excitation control - vf*)
- the active power consumed by the impedance load at bus 2
- the active power consumed by one of the motors at bus 2
- the speed of one the motors at bus 2.

From RAMSES outputs, determine the current in line 3-4 during the short-circuit. Consider the value just after fault occurrence, for security. Check this value with a simple circuit calculation involving the generator equivalent circuit.

Case 5

- Operating point : # 2
- disturbance : at $t = 1$ s, tripping of **both** circuits of line 1-3 (without fault)
- simulated time : 25 s.

Comment as far as possible the evolution of :

- rotor speed of G5
- active power produced by G5
- control valve opening
(select: generator G5 - observable of torque controller - z)
- turbine mechanical power
(select: generator G5 - observable of torque controller - Pm ;
in pu on the turbine nominal power).

Compute the final rotor speed using a formula from primary frequency control.
Comment on the accuracy and try improving it.

Case 6

- Operating point : # 2
 - disturbance : at $t = 1$ s, a solid fault on line 1-3, cleared after 10 cycles (0.20 s) by opening the faulted circuit. The fault takes place very near bus 3, so that it can be applied at bus 3
 - simulated time : 20 s.
-
- Observe that the voltage at bus 3 does not recover near 1 pu, but stays “locked” near 0.84 pu². Find which system component is responsible for this, with the help of the proper curves
 - show that for some shorter fault duration (i.e. smaller than 0.20 s), the voltage does not stay “locked” at such a small value. Explain the underlying instability mechanism.

²this is a totally unacceptable value ! The system is considered unstable

Case 7

- Operating point : # 1
 - disturbance : at $t = 1$ s, severe disturbance in the external system simulated by a decrease of the Thévenin voltage by 0.2 pu in 1 s (the voltage remains at its low value)
 - simulated time : 120 s.
-
- Explain why the voltage at bus 3 drops so much after some time.